Laser Interferometer LP30 -3D

User manual
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Laser measurement system *LP30-3D* is a two frequency interferometer intended to be used mainly in machine geometry measurements. Its small size and low weight simplify transportation and make the instrument especially useful for service applications. Software version for Windows 9x/NT/2k/XP and automation of many measurement processes make the interferometer easy to use. Software, compliant with ISO/DIS 230 and PN–93 M55580, enable making rapports and diagrams. It is possible to choose statistical results processing according to norms: ISO 230-2 (European), VDI/DGQ 3441 (German), NMTBA (USA), BSI BS 4656 Part 16 (British) and PN-93 M55580 (Polish).

Very good technical parameters of the interferometer allow using it also in scientific laboratories, for precision positioning, for scaling optical and magnetic liners, etc.

**Safety considerations**

The Laser Interferometer *LP30-3D* is a Safety Class I product designed and tested in accordance with international safety standards. It is also a Class II Laser product conforming to international laser safety regulations. The
instrument and the manual should be inspected and reviewed for safety markings and instructions before operation.

Warnings

Although the laser measurement system LP30-3D was designed to be used in harsh environments, the following conditions must be met:

- The laser head must not be put near strong magnetic fields.
- The head should not be unscrewed from its base and if it is, it may not be put on a heat sink (e.g. thick metal plate).
- The head must not be thrown or dropped.
- Keep the optical components clean and avoid scratching them.
- When the optics is dusted, clean it with pure alcohol.
- Do not use the system beyond its work conditions.
The rules of laser displacement measurements

Displacement measurements with the use of a laser interferometer allow obtaining the accuracy of an displacement measurements of 0.4 ppm in air and 20 nm in vacuum. The interferometer was first built by A.A. Michelson in 1881. The simplified schematic of the interferometer is shown on fig. 2.1.

Coherent light beam falls on a semi-transparent mirror. This mirror splits the light into two beams. The first goes to the reference arm and reflects from the reflector Z₁; the second goes to the measurement arm and reflects form the reflector Z₂. The reflected beams meet again on the detector. Because these beams come from the same, coherent, source, they will interfere. When the moving reflector is being displaced, the frequency of the reflected beam in the measurement arm changes. The detector counts the frequency difference between reflected beams - \( f_D \) (see fig. 2.1). The measured value of the displacement is calculated according to

\[
L = f_D \frac{\lambda}{2} = N \frac{\lambda}{2}
\]

Where: 
\( N \) – number of pulses,
\( \lambda \) - light wavelength.
The construction of real interferometers

The main disadvantage of Michelson interferometer results from the fact that the detector cannot determine, whether $f_D$ is negative or positive thus, from the measurements the displacement of the moving reflector without the sign is obtained. Currently there are widely used two methods that allow getting also the direction of the movement. Depending on the number of light frequencies (wavelengths) used in the interferometer, the first is called homodyne (one frequency) and the second heterodyne (two frequencies) method.

In the homodyne method, shown on figure 2.2, as a coherent source of light a linearly polarized laser is used. If it is two-mode laser (i.e. it generates two wavelengths) than one mode must be cut off with the use of a properly set polarizer. The polarising splitter splits the light beam from the laser into two
beams polarized vertically (90°) and horizontally (0°). The former is directed to the measurement arm and the latter to the reference one. The frequency of the beam in the measurement arm changes with the movement of the moving reflector. The polarization of the reflected beams is changed to circular with the use of a $\lambda/4$ waveplate. After 0° and 45° polarizers, two signals shifted in phase are obtained. The phase shift is +90° when the measurement arm moves to and -90° when it moves from the laser.

**FIG.2.2. THE BLOCK DIAGRAM OF AN INTERFEROMETER WORKING ACCORDING TO THE HOMODYNE METHOD.**

In the heterodyne method, shown on figure 2.3, two laser frequencies are used. Therefore a two-frequency laser is needed, e.g. a Zeeman laser. A two-
mode laser is not suitable for the heterodyne method interferometer, because the difference between \( f_1 \) and \( f_2 \) is usually too high for an electronic counter. The output beam of a Zeeman laser consists of two circularly polarized beams, one polarized leftward and the second rightward. A \( \lambda/4 \) waveplate changes circular polarization to linear. The main difference between two described methods is that in the heterodyne one the beam frequency in reference arm differs from the beam frequency in the measuring arm. A detection path is also different – subtracting differential frequencies of reference and measuring arms does the measurement.

**FIG. 2.3.** THE BLOCK DIAGRAM OF AN INTERFEROMETER, WORKING ACCORDING TO THE HETERODYNE METHOD.
The heterodyne method gives correct results only when $f_D$ does not exceed the difference between the laser frequencies, i.e.: $f_2 - f_1$. In reality, that difference, resulting from the Zeeman effect, is about 1MHz. This limits the maximum available velocity of measuring arm, in one direction, to 0.3 m/s. The next disadvantage of the heterodyne method is, that two frequencies must be used for measurements, while in the homodyne method the second may be used for measuring e.g. a second axis.

The influence of the outside conditions on the measurement accuracy

According to equation (1) an interferometer’s unit of measure in length measurement is laser’s wavelength. From definition

$$\lambda = \frac{v}{f} \quad (2)$$

A wavelength depends on laser’s frequency $f$ and the speed of light $v$ in the measuring path. If the measurement is done in vacuum, than $v = c = 3\times10^8$ m/s. The speed of light in a medium other than vacuum (e.g. air, water) is lower and is described as

$$v = \frac{c}{n} \quad (3)$$

Where: $n$ – a refraction coefficient.

Normally the refraction coefficient $n$ is a complex variable or even a tensor, but for less accurate calculations it is simplified to a constant. The air coefficient depends mostly on the pressure $P$, temperature $T$ and humidity $H$. 
The dependence \( n_{T,P,H} \) for the air was empirically determined by Edien and is described as

\[
n_{T,P,H} - 1 = 2,8775 \times 10^{-7} \times P \left( \frac{1 + 10^{-6} \times P \times (0,613 - 0,00997 \times T)}{1 + 0,003661 \times T} \right) + \Delta n
\]  

(4)

\[
\Delta n = -3,033 \times 10^{-9} \times H \times e^{0,057627 \times T}
\]  

(5)

From the above equations one may obtain the refraction coefficient dependences on T, P and H in usual conditions (T=293K, P=1000hPa, H=50%):

\[
\frac{\partial n}{\partial T} = -0,93 \times 10^{-6} \left[ \frac{1}{K} \right]
\]

\[
\frac{\partial n}{\partial P} = +0,27 \times 10^{-6} \left[ \frac{1}{hPa} \right]
\]

\[
\frac{\partial n}{\partial H} = -0,96 \times 10^{-8} \left[ \frac{1}{\%} \right]
\]

It is worth to notice that the most critical parameter is the temperature, because its change influences the coefficient \( n \) more than changes in the pressure and much more than changes in the humidity.

The accuracy of laser interferometers

*Errors caused by the environment*

The most impotent source of errors in machine geometry measurements is the temperature (or more exactly, the change of the temperature) of the measured machine. For example, if the machine’s base is made of steel, than the base’s length increases 11.7\( \mu \)m when its temperature changes 1K. It shows how important it is for very precise measurements to measure the temperature of the controlled part of the machine and to use it in readout corrections. This is not a
simple task for a few reasons, but the most important one is that, than when the machine operates, there are temperature gradients on it. That means that more than one temperature sensor is needed and that the more sensors are used the better accuracy can be achieved. Moreover the shape of the measured part of the machine may “absorb” a part of the expansion of the material or the part may be built of materials of different expandability.

As was mentioned in the previous chapter, the temperature influences the accuracy also as it changes the refraction coefficient of the medium the measurements are made in (usually it is air, but may be e.g. water). An Edien equation was presented, showing how the refraction coefficient of the air changes with the change of the air temperature, pressure and humidity. The errors caused by the change of the wavelength are less important than the mentioned above, but they cannot be abandoned. Roughly, a 1ppm error (i.e. 1µm/m) is caused by: the air temperature change of 0.1K, the air pressure change of 4hPa and the air humidity change of 30%.

A dead path error

A dead path error is an error associated with the change in environmental parameters during a measurement. This error occurs when some part of the light path (a dead path) is not included in the temperature (both air and base), pressure and humidity compensation.

The dead path of the light path is a distance between the optical interferometer and the base (or the null point) of the measuring position (L₁ on figure 2.4). Let the position of the interferometer and the retro-reflector do not change. When there is a change in the air temperature, pressure or humidity, than the wavelength changes on the whole path length (L₁ + L₂). The path length changes also when the temperature of the base changes. But the correction system will use the correct wavelength only on the length L₂ and will correct
only this length. The correction will not be made on a dead path $L_1$. In this way, the laser system will “move” the base point.

A dead path error is the more severe the greater is the distance between the interferometer and the base point. This error is especially important in laser interferometers where the interferometer is build-up in a common casing with a laser head, because it is than very difficult to reduce a dead path.

![Diagram of a dead path error](image)

FIG.2.4. AN ILLUSTRATION OF A DEAD PATH ERROR.

A cosine error

If the laser beam is not parallel to a measured axis of a machine (i.e. the optical path is not properly adjusted) than a difference between the real distance and the measured distance occurs. This error of unadjustment is known as a
cosine error, because its magnitude depends on the angle between the laser beam and the axis of the machine (fig. 2.5).

If, as a reflector a flat mirror is used, than the beam must be perpendicular to it. If the machine changes its position from point A to point B, than the beam stays perpendicular to the mirror, but moves on its surface. The distance measured by the laser interferometer $L_{LMS}$, will be smaller, than the real distance $L_M$, according to

$$L_{LMS} = L_M \cdot \cos \Theta$$  \hspace{1cm} (6)

The above equation is valid also when as a reflector a corn cube is used.

**FIG.2.5. THE BEAM UNADJUSTMENT AS A CAUSE OF A COSINE ERROR.**

The only method of eliminating the cosine error is a proper laser beam adjustment done before a measurement.
**An Abbe error**

An Abbe error occurs when, during measurements, the measured part does not move perfectly straight and there appear angular movements, which cause sloping of the retro-reflector. The sloping of the reflector is the greater the longer is the distance between the axis of the measurement and the axis of movement. This distance is called *An Abbe offset*. Only the movements in the axis of the measurement are important (see fig. 2.6). An Abbe error may be avoided only when there are no angular movements of the retro-reflector in the axis of the measurements.

![Fig. 2.6. An illustration of an Abbe error.](image-url)

**A laser stability error**

As was already mentioned, in laser measurements the laser wavelength instability changes directly the readout from the interferometer, e.g. a relative instability of the laser in the range of 1ppm ($10^{-6}$), causes an error of 1µm on every 1m of a measured distance. Therefore the laser instability error is important mainly in measurements in vacuum (where a refraction coefficient is...
constant) and when a low stability laser is used (e.g. a semiconductor laser). The stability of usually used in laser measurement systems, HeNe gas lasers is 0.02 ppm, so the stability error may be neglected.

Other errors

In some conditions, a noticeable error may be caused by the electronic part of the interferometer. As the electronics is used mainly for counting, the errors may be associated either with miscounting (some pulses are not counted) or with miscalculating (the calculations are made with finite precision).

A summary of laser measurement system errors

In order to show which of the errors influence the accuracy of a laser measurement system the most, an exemplary calculation of errors on a 1m long steel machine is shown on figures 2.7 and 2.8. Different scales of the charts should be taken into account.
FIG. 2.7. A CALCULATION OF ERRORS FOR A LASER MEASUREMENT SYSTEM WITHOUT THE COMPENSATION OF THE ENVIRONMENT.

FIG. 2.8. A CALCULATION OF ERRORS FOR A LASER MEASUREMENT SYSTEM WITH THE COMPENSATION OF THE ENVIRONMENT.
To start the measurements using the Laser Interferometer *LP30-3D*, software "LP 30 -3D" should be installed on HDD of a PC computer. The hardware requirements are:

- Windows 9x/NT/2k/XP system,
- CR-ROM
- Pentium processor, 90 MHz or better
- SVGA graphic card making possible working with resolution 800x600.

Software installation

To install the LP program on the PC computer put the CD disc "LP30-3D" into the CD-ROM. The program will be installed automatically.
The Laser Interferometer system elements

The number of elements the system consists depends on desired types of measurements. To the standard set (for linear measurements) belong:

1. 1 x Laser head – *Laser Interferometer*
2. 1 x Power supply - *Laser Interferometer Power Supply*
3. 1 x Tripod stand
4. 1 x Environmental Compensation Unit - (ECU)  **SM1**
5. 1 x Laser head to power supply cable
6. 2 x Magnetic holder **UM1**
7. 1 x Linear interferometer **IL1**
8. 1 x Linear retro-reflector **RL1**
9. 3 x Basis temperature sensor **T1, T2, T3**
10. 1 x RS232C cable
11. 1 x Manual Strobe cable

See fig. 3.1 on the next page for pictures of the elements of the standard set.

Additional elements for angular measurements are:

1. 1 x Angular interferometer **IK1**
2. 1 x Angular retro-reflector **RK1**
3. 2 x Beam directing mirror **ZK1**
4. 1 x Rotary table **SO1**
Fig. 3.1. The elements of the standard set.
4

OPERATION

Preparing the interferometer to work

The Laser Interferometer LP30-3D is supplied from autonomous power supply – „Laser Interferometer Power Supply“. Communication with a PC computer is performed by the RS 232C or USB interface. Before starting the measurements place the laser head – "Laser Interferometer“ on the Tripod stand and connect it with the LP power supply. Connect cable from laser head to socket on the front panel of the "Laser Interferometer Power Supply". Connect the RS 232C/USB cable to DB9 male socket on the front panel of the Power Supply. The second end of the cable plug into the RS 232C socket of the computer or, with additional RS323-USB interface, to USB socket of the computer.

Connect the Environmental Compensation Unit - (ECU) (TPH) to 6-pin marked METEO socket on front panel of the Power Supply. Temperature sensors T1, T2, T3 connect to 4-pin sockets placed on the front panel. To 6-pin socket marked STROBE should be connected a source of strobe signal. Strobe signal may be produced by a pulse switcher (5 m cable with a pulse switcher is in standard set) or by any other devices. Strobe input is used to control the moment of measurement either by hand or at dynamic positioning.
Turning the system on

Switch on the device according to the following instructions:

1) Switch on the power switch on the Laser Interferometer Power Supply,
2) Start LP30 program on a computer.

When the main menu appears at the computer monitor (fig.4.2) choose option **Display** (fig.4.4)

If the program is started before the Power Supply is turned on, or the Power Supply is not connected properly to the computer, on the monitor an error
window with “No connection or Power Supply Off” line will appear (fig. 4.3). To get rid of this error quit the program, check the connection and/or the supply of the Interferometer (the POWER diode should be on).

![FIG.4.3. ERRORS THAT MAY OCCUR DURING SOFTWARE LOADING](image)

If the Interferometer is connected to the wrong COM than an error window with “Could not open COM port. Check COM port settings” line will appear. To change the number of used COM port choose option Config (fig 4.4).

Getting basic information from the system.

After proper software loading choose option Display. The laser system will be preheated. The beam intensity – the green indicator on the screen – will appear and disappear. The speed of changes will become smaller due to the increase in the temperature of the laser system cover. The measuring system is ready for an adjustment of the optical arrangement of the laser path.
On the Display screen there are four panels:

- Panel containing the digital result of the measurement, the measuring signal level indicator and the buttons for changing the number of displayed **Digits** and for changing **Units**. Quantity of significant digits on display may be changed with the use of buttons ↑↓, pressing button with an inscription **Change** changes measurement unit on the display. In the upper left corner there is an icon making link to Microsoft Excel (if installed). Running this link allows to register measurement in Excel cells by each STROBE button press.

- Panel **Environmental** where measuring data obtained from the Environmental Compensation Unit - (ECU) are shown. On the screen there are shown: temperature, pressure and humidity of the atmosphere and temperatures measured by three base temperature sensors. Average temperature of the base measured by three sensors is also presented.
- Panel **Measurement** contains basic information about conducted measurement. With the left button the type of measurement may be changed. The right is used for choosing measuring axis. At every changing of measuring option (i.e. distance, speed, angle, straightness) and changing of measuring axis (i.e. X, Y, Z) a drawing suggesting the arrangement of the optical elements appears on the screen. Clicking with left mouse key in the area of the drawing causes showing of help on a theme of optical arrangement adjustment.

- Panel **Parameters**, contains a few options. Option **Sign** allows choosing whether enlarging distances between the retro-reflector and the interferometer gives positive (default “+”) or negative result on the display. In the option **Material** one can choose the material from which a basis of a machine is made of, the value of the thermal expandability coefficient of the basis is accepted for calculations of compensation. Option **User** make it possible to enter any value of the thermal expandability coefficient. In the panel **Resolution** one can change between high (10nm) and low (100nm) system resolution. In higher resolution accepted movement velocity is strictly limited (see Technical data chapter for details). With the option **Environmental** the Environmental Compensation Unit - (ECU) may be switched on or off. From console of the computer one can switch off the external Environmental Compensation Unit - (ECU) and insert the parameters of atmosphere by hand.

When measurements are executed with automatic compensation of the atmosphere parameters and compensation of the basis temperatures (Environmental Compensation Unit - ECU switched on) one should:

- Place the Environmental Compensation Unit - (ECU) on the machine in the vicinity of the laser beam.
- Place the sensors of the basis temperature along the measured axis on the machine basis

Measurement executed without automatic compensation are referred to normal conditions: temperature 20 °C, pressure 1016 hPa, humidity 50 %.
Adjustment of the optical path

An adjustment of the optical set up should be conducted in option Display. It can be done during laser head heating. Final check should be made when the system is ready to work.

The Laser Head should be firmly attached to the tripod. The tripod should not touch a machine as it may cause vibration of the laser head and the optical path. Turn special attention, not to move the legs of the tripod during the measurements, because it will cause shift of elements of the optical path and the necessity of repetition of the adjustment process. The arrangement of the tripod helps to adjust the optical path. Inspection of the level of arrangement can be made using level fastened on the tripod and on the laser head.

The diaphragm of the laser beam is found on the front panel of the laser head. The diaphragm can be placed in three positions:

- Right extreme position (fig. 4.5a) – "Adjustment" – the laser beam goes out through opening in the diaphragm about 2 mm diameter,
- Central (fig. 4.5b) – "Measurement" from the laser head goes out beam about 8 mm diameter,
- Left (fig. 4.5c) - extreme position, in which the exit of the beam from the laser head is completely closed.
During transportation or when system is not used, correct position of diaphragm is left extreme position. In this position optics is safe from getting dirty, covering with dust and accidental damage during transportation.

Basic rules of an optical path adjustment:

When the position of the laser beam is being corrected, the spot position on the diaphragm of the interferometer (the interferometer is placed closer to the laser head) – should be regulated with X stage and up-down translation stage Z and up-down translation of the tripod. The spot position on the retro-reflector diaphragm (the retro-reflector is far from laser interferometer) – should be regulated with “α” angle adjustment in vertical and “β” angle adjustment in horizontal line. The regulating elements of the laser head are presented in fig. 4.6. In Fig. 4.6d one can see the position of the laser head for Y axes measurement. In this position the function of the regulating elements will changed.
Adjustment process

1. In the option **Display** in the PC program choose type of measurement, which will be done and axis along of which measurements will be carried. On the screen will appear a drawing showing recommended arrangement of measuring elements at the chosen type of measurement.

2. Linear interferometer IL1 and linear retro-reflector RL1 should be mounted on magnetic holders UM1, UM2. Regulating elements of the laser head should be placed in central positions, to assure maximum range of regulation.

3. Choose which from the optical elements will be moved (retro-reflector RL1 or interferometer IL1) and attach both with magnetic holders: one to a moving element of the machine, second to an element in relation to which displacement will be measured (for example: the retro-reflector may be fasten to a moving element, and the interferometer to a motionless table). Remember, *that relative linear displacement between the retro-reflector and the interferometer is measured.*
Attention! It is inadmissible to place one of optical elements (i.e. RL1 or IL1) outside the machine on an additional stand – the system measures then also displacements of the machine in relation to the stand).

4. The moving element of investigated axis should be moved in closest position to the laser head position

5. Place the interferometer optics IL1 and the retro-reflector RL1 on the axis of movement. Check the level indicator that the interferometer is in horizontal position.

   Attach the retro-reflector RL1 to the interferometer IL1 (there is a special socket for this purpose in IL1) – see fig.4.7.

   6. Move the moving element of the machine together with the attached optical element in opposite extreme position. Diaphragms on IL1 and RL1 and of laser head place in position – “Adjustment”.

FIG.4.7. START POSITION OF ADJUSTMENT
7. Regulate the tripod height and level of the laser head by means of a sphere joint. The laser beam has to fall on upper hole in interferometer diaphragm and after passage by the hole must be found within diaphragm area of the retro-reflector. The laser head should be placed horizontally (for horizontal axes) – control it on the level indicator.

8. Using regulating elements of the laser head find a position in which laser beam passes through both upper apertures in the diaphragms placed on the interferometer and the retro-reflector.

9. Switch the diaphragms on IL1 and RL1 in a position of work.

10. Using the regulating elements of the laser head adjust the position of laser beams on the diaphragm of laser head. Two return beams should exactly cover each other an entrance hole on the front panel of the laser head. If this is necessary gently correct the position of the IL1. Shift the diaphragm on the laser head to the position “Work”. The level of the measuring signal (the green indicator on the screen of the computer) should have value not less than 80 % during translocation of the moving element along whole path.

11. For precision adjustment, when the straightness measurement will be carried on, use electronic adjustments. Switch screen of the display to Adjustment mode. Using adjustment screw set two crosses blue and green to the
centre of the screen. Blue cross corresponds to reference beam while the green one to measuring beam see Fig 4.9.

**FIG.4.9. CORRECT ADJUSTMENT OF OPTICAL PATH**

12 Reset displayed position using “Reset” button on the display. System is ready to work.

**Attention!** Remember, that the position when the interferometer touches the retro-reflector can serve only to adjust. Be sure that during measurements in extreme nearest measuring position the retro-reflector does not touch the interferometer, because it can be a source of measuring errors.
Measurement set

Linear measurements are the most often used measuring option. Using this option it is possible to measure:

- Linear displacement;
- Velocity of moving element;
- Linear positioning.
- Vibrations (see Chapter 8);

Measurements may be executed in three mutually perpendicular measuring axes X, Y, Z. Change of a measured axis will demand displacements of optics.

Required measuring set: a computer, a laser head with a power supply, a stand Tripod, two magnetic holders UM1 (or two UM2), a Environmental Compensation Unit (ECU) - SM1, sensors of basis temperature T1, T2, T3, a linear interferometer IL1, a linear retro-reflector RL1, remote control Strobe (option).
**FIG. 5.1** SET UP FOR LINEAR MEASUREMENTS IN X AXIS.

**FIG. 5.2.** SET UP FOR LINEAR MEASUREMENTS IN Y AXIS.
Linear displacement measurement

When one want prepare the measurement system for the measurement of a linear displacement electric connections and adjustment of the optical path (see chapter 4) must be carried out. When the laser system is ready to work – green LED light on the forehead of the laser head. Next it is necessary to check optical path, i.e. whether the measuring signal reached at least 80% on the entire axis. The measurements now can start. A measuring unit (mm, µm), a number of significant positions on a display, a measured axis, a sign (“+” or “-“) and base’s material may be chosen. After resetting, the display system is ready for measurements. When the retro-reflector is moved, on the screen the displacement in relation to a starting point is displayed (it is also possible to move the interferometer in relation to the standing retro-reflector).
Linear displacement velocity measurement

The arrangement of the optical path and the laser head should be the same as in the paragraph above. The measurement of the linear displacement velocity is executed in option Display. The type of measurement should be changed on Velocity and a unit should be chosen (m/min, m/s). After resetting the result on the display, system is ready to the velocity of displacement measurement. During translocation of the retro-reflector the value of velocity is presented on the screen (is possible to measure velocity moving the interferometer in relation to motionless the retro-reflector).

Velocity graph

The arrangement of the optical path and the laser head should be the same as in the paragraph above. It should be activated Main Menu and chosen option Velocity. Than a button Start should be pressed and the object, which displacement velocity we investigate, should be moved. After moving stop button Stop should be pressed. On the screen will appear a graph of velocity. Clicking on a part of the graph and moving the mouse rightward we receive increasing of a selected fragment of the graph. Clicking on a part of the graph and moving mouse leftward we cancel increasing. The graph can be printed or saved to file when we choose from upper menu File, and then suitable option (i.e. Save, Save as, Print).
An example graph of changes of the linear displacement velocity of a machine table in one axis is presented on fig. 5.5.

**FIG.5.4. VELOCITY GRAPH WINDOW.**

**FIG.5.5. EXAMPLE GRAPH OF CHANGES OF LINEAR DISPLACEMENT VELOCITY.**
Program also counts an average velocity from a visible range on the graph. Possible is also presetting of minimum and maximum values for measured axis. Clicking left mouse button on selected axis or clicking right mouse button within the area of the graph appears a menu, from which we choose proper axis. On the screen appears a window of scaling of axes **Velocity scale** and **Time scale**. We can place scaling automatic or set maximum or minimum values.

Program makes possible also saving the velocity graph and then loading it for example to Word editor. To save graph to file we should click with right mouse key within the area of the graph. Popup menu will appear menu from which we should choose **Copy to clipboard** instruction.

The choice of the speed unit is also possible: from menu **Edit** we should choose option **Config**, where we can set the velocity unit.

Linear positioning measurement

The linear positioning measurement is the most advanced option of linear measurements. It is most common form of measurement performed on the machines. The system measure linear positioning accuracy, repeatability and backlash by comparing the position displayed on a machine’s readout with the true position measured by the interferometer. In order to start measurements option **Main Menu** should be activated and **Positioning** should be chosen. On the screen will appear a window **Linear positioning** as presented on fig. 5.6
In this window appears upper menu, which consists of options: File, Edit, Measurement, View, Help. In option File are found instructions making possible reading measuring data from disc, saving data on disc and printout of measurements results. Option Edit allows to enter measured machine parameters, preview of measurement results in every cycle of positioning and an edition of positioning points (when option Target Points from List from menu Measurement is active).

Option **Measurement** includes the options connected with the process of measurement:

- **Start** – beginning of measurements
- **Stop** – break of measurements
- **Dynamic** – choosing this option activates dynamic mode of linear positioning measurement.
- **Manual Capture** – choosing this option causes, that for measuring points we can get measured value of displacement by pressing a button **Manual**
**Capture** or by pressing pulse switcher of Strobe. If this option is not active points are captured automatically (program detects the moment of machine stop).

**Target Points From List** – after choosing this option on the screen appears a window for edition measuring points in which we write or count distance value for positioning points. If this option is not active then the positioning points are marked automatically in first measuring cycle.

**Stop After Cycle** – if this option is active program breaks the measurement after realization of a measuring cycle and if it is not active number of cycles set in configuration is executed.

**Change Given Values** – setting this option gives possibility to change an earlier defined distance value of a measuring point during the measurement process. Before point capture appears a window in which can be written new distance value whereupon marked are only places after comma what causes that it is not necessary to write all distances.

Option **View** serves to switching on or off a panel **Target Position, Error Table** and to switching on drawing on the graph of measuring points from all cycles (active cycle is drown using solid line but remaining cycles are illustrated using only points).

If system is ready to work, then on the screen appear two digital displays and gauge of measuring signal level. On the upper display measured value is shown, on the bottom display value of target position, which is read from data points table or appointed automatically. Under the displays from the left side there is presented a graph on which the results of measurements are shown. From the right side **Error Table** is found. Under the graph button **Start** - beginning measurement and button **Main Menu** - allowing to enter to Main menu are placed.
In the bottom parts of the window a status bar can be found, on which there is presented a configuration of the positioning measurements. In the first field information about method of measuring points capture is found (manual, automatic). In second field information whether measuring points originate from list or are marked automatically is shown. The next field informs about number of cycles in series (number of cycles executed one after one, if not active is option Stop after every cycle). In the last field information about activity of option Stop after every cycle is presented.

To execute the linear positioning measurement program has to know the target position in which it has to make measurement and to count deviation. These can be automatically defined in the first measuring cycle on a condition that distances between points are marked with accuracy to full millimetre. The positioning points can be also written or counted after marking an option Target Points From List. After activating this option the positioning points can be defined in any accuracy.

Measurement can be driven in an Automatic option or in a Manual Capture option. In automatic version the system oneself recognizes the moment of stop, the value of target point, the direction of movement and the number of series.

For correct work of automatic option below rules should be used:
1) Time of stop duration in measuring point - at least 1 second,
2) Vibrations of machine - not too large.

If vibrations are too large – system does not capture points – then the option Manual Capture should be switched on in the menu Measurement. After choosing the Manual Capture option on the bottom of the screen appears an additional button Manual Capture. Capture of the measuring point takes place by pressing this button or pressing the button on the impulse switcher.

Examination of linear positioning of machine consists of at least 2 measuring cycles. In every cycle the measured machine will move the retro-
reflector for programmed distance fore (Avers) and back (Revers). After each shift the machine should stop for a time at least one second. The measured distance by the laser system is saved in the table of results. After at least two series of measuring cycles, statistical calculations can be executed and execute-report from examination is prepared. In order to get the final report press a button **Report**. Using buttons **Remove** and **Add** it is possible to change the measuring cycle in which accidental error is suspected. The screen of the computer after pressing the button **Report** is presented on fig. 5.7

![FIG.5.7. LINEAR POSITIONING RESULTS.](image)

The positioning parameters are presented on the graph. In the right side panel **Results** is found, on which results of statistical calculations and a norm according to which calculations were executed are presented. The norm can be chosen from a list. After choosing a new norm the results are recalculated.

Under the graph buttons used for the change of the axis scale **Axis Scale** (automatic scaling or assignment, minimum and maximum values), choosing of
parameters shown on the graph **Parameters**, report, printout **Print** and return to looking through the measuring **cycles Previous Menu** are found.

Example of linear positioning report of CNC machine in axis is presented on fig. 5.8

---

**POSITIONING RAPPORT**

<table>
<thead>
<tr>
<th>Machine: BFK130</th>
<th>Serial No:</th>
<th>Axis X</th>
</tr>
</thead>
<tbody>
<tr>
<td>File Name: BFK130X1.d2</td>
<td>Acquisition date: 01-11-08 15:41:14</td>
<td>Current date: 02-11-06 15:08:15</td>
</tr>
</tbody>
</table>

| Measurement System: LSP-30 Compact | LASERTEX |

<table>
<thead>
<tr>
<th>Results</th>
<th>Measurement Conditions</th>
</tr>
</thead>
<tbody>
<tr>
<td>Norm: NMTBA</td>
<td></td>
</tr>
<tr>
<td>Accuracy:</td>
<td></td>
</tr>
<tr>
<td>Forward:</td>
<td>59.6 µm</td>
</tr>
<tr>
<td>Reverse:</td>
<td>63.5 µm</td>
</tr>
<tr>
<td>Bidirectional:</td>
<td>61.5 µm</td>
</tr>
<tr>
<td>Repeatability:</td>
<td></td>
</tr>
<tr>
<td>Forward:</td>
<td>16.4 µm</td>
</tr>
<tr>
<td>Reverse:</td>
<td>20.1 µm</td>
</tr>
<tr>
<td>Bidirectional:</td>
<td>13.2 µm</td>
</tr>
<tr>
<td>Backlash:</td>
<td></td>
</tr>
<tr>
<td>Mean:</td>
<td>-0.4 µm</td>
</tr>
<tr>
<td>Max:</td>
<td>2.6 µm</td>
</tr>
</tbody>
</table>

---

**FIG.5.8 LINEAR POSITIONING REPORT**
Recording mode

The long term changes of the length of machine axes under changes of temperature condition may give the information about thermal properties of the machine. This kind of measurements called “Recording mode” may be chosen by pressing RECORD button on the Display screen. This switches the system into the mode of the data recorder. The time interval of the records could be programmed from the computer by setting a required value.

Pressing “End Recording” finishes the data recording. The results can be saved with the choice of “Save to file”. In fig. 5.9 the example of Data Record is presented.

**FIG.5.9 RECORDING DATA MODE.**
Measuring set for angular measurements

The angular measurements performed by the laser interferometer system are used for straightness, surface flatness and angular positioning of rotary tables. Straightness measurements can be done in three mutually perpendicular axes X, Y, Z.

**FIG. 6.1. SETUP FOR ANGULAR MEASUREMENTS IN X-AXIS.**
Change of measuring axis will demand displacements of angular optics (figures 6.1, 6.2 and 6.3)

**FIG.6.2. SETUP FOR ANGULAR MEASUREMENTS IN Y-AXIS.**

**FIG.6.3. SETUP FOR ANGULAR MEASUREMENTS IN Z-AXIS.**

Required measuring set: a computer, a laser head with an interferometer power supply, a stand Tripod, two magnetic holders $UM1$ (or $UM2$), a
Environmental Compensation Unit - (ECU) SM1, sensors of basis temperature T1, T2, T3, an angular interferometer IK1, angular retro-reflector RK1 mounted on P100 mm base, remote control Strobe (option).

Auxiliary equipment used in the angular measurements is: two mirrors ZK1 mounted on supports, serving to reflect the laser beam - necessary to measurements of the surface flatness; a rotary table SO1 controlled by step motor - used to angular positioning measurements.

Measurement of angle deviations

Preparations to measurements are similar to those described in the previous chapter. The measurements are executed in Display mode. The type of measurements should be set to Angle and a suitable measured axis should be chosen (fig. 6.4). It is accepted that when the retro-reflector is bent towards the laser head direction, measured value is positive. It is possible to change the sign in the option Parameters – Change of sign.

FIG.6.4. ANGLE DEVIATIONS MEASUREMENT SETUP.
After display reset the system is ready to measurements. If the retro-reflector is moved to a new point and on the screen the value of the angle deviation in relation to the first point is shown. It is also possible to measure change of the angle deviation in the same point if the inclination of retro-reflector changes.

**Straightness measurements**

The straightness measurements are driven along a straight line to which side surface of the angular retro-reflector base is tangent. In order to get the correct measurement the straight ruler, along which retro-reflector base will be pushed, should be fasten on a measured axis. In every moment of the measurement side surface of the retro-reflector base should be tangent to the ruler (see fig. 6.5).

**FIG.6.5. AN EXAMPLE OF OPTICAL COMPONENTS SETUP IN STRAIGHTNESS MEASUREMENT.**
Required measuring set: a PC computer, a laser head with a laser interferometer power supply, a stand Tripod, two magnetic holders UM1 (or UM2), a Environmental Compensation Unit - (ECU) SM1, sensors of basis temperature T1, T2, T3, an angular interferometer IK1, an angular retro-reflector RK1 on a support base P100 mm, a remote control Strobe.

The Straightness measurement is based on pushing angular retro-reflector about an interval 100 mm and measuring its angle deviation. Before accession to the measurement, measuring points should be marked every 100 mm distance on the leading ruler or on the examined surface. It is recommended using ruler with scale. The straightness measurement is performed in the option Straightness, chosen from Menu Main (fig. 6.6).

The measurement can be done in an automatic mode (standard arrangement) or in a manual mode with manual capturing of measuring points.

In the automatic mode capturing of the measuring points takes place when a temporary time interval runs out. The time between capturing the measuring
points is used to move the retro-reflector about a distance of 100 mm. The time interval should be used in dependence from practices of a person leading the measurements. It is suggested to set the time on 10 s and to decrease it if needed. An arrangement of the time interval may be done by pressing ←, → keys on the computer screen. The retro-reflector base P100 should be placed at the beginning of the examined axis close to the interferometer. After the Start button is pressed one should wait on capturing the first measuring point. Then one should move the retro-reflector base of about 100 mm and to wait on the next point capture. Announcements shown on the computer screen make the measurement easy. After capturing the last measuring point press Stop.

If from some reasons will not be possible to move the retro-reflector base before the capture moment, the measurement should be repeated from the beginning point and possibly the measuring interval should be enlarged.

![FIG.6.6. A RESULT OF STRAIGHTNESS MEASUREMENT.](image)

To make the measurement in the manual capture of the measuring points, the **Measurement automatic** in option **Measurement** should be switched off.
The measurement begins by pressing **Start**. The Capture of the measuring points can be done from the computer keyboard or by pressing the remote Strobe button. Each time after the movement of the retro-reflector base of about 100 mm measuring point should be captured. After capturing the last point **Stop** should be pressed.

The results of the measurements may be saved to a file or printed in dependence of the options in the menu **File**.
Preparations

The flatness measurement is done on the basis of straightness measurements of eight axes. From obtained data a flatness map is drown. (fig. 7.1.).
Required measuring set consists of: a PC computer, a laser head with a power supply, a **Tripod** stand, two magnetic bases (UM1 and/or UM2), a Environmental Compensation Unit - (ECU) **SM1**, basis Environmental Compensation Unit - (ECU) sensors (T1, T2, T3), an angle interferometer **IK1**, an angle retro-reflector **RK1** on a base **P100** and two beam directing mirrors **ZK1**.

The element set for the flatness measurements is shown on fig. 7.2.

**FIG.7.2. THE ELEMENT SET FOR THE FLATNESS MEASUREMENTS (IK1, RK1 ON P100 BASE AND ZK1)**

Adjustment of optics for the flatness measurements

The measurement of flatness consists of the measurements of deviations from straightness made along 8 axes. The measurement axes are set on a measured surface as shown on figure 7.3. On this figure are shown also:
directions of measurements in the axes and margins that must be kept during measurements.

The measurements of deviations from straightness are made with angular optics as described in Chapter 6, *Straightness measurements*. Depending on the measurement axis, a different set of optical components is used and the adjustment of the optical path is done in slightly different way. All flatness measurements are done with one laser head position, shown on Figure 7.3.

The flatness measurements are performed in the option **Flatness**. chosen from the **Main Menu**. After setting proper base length (standard is 100mm) and machine data (Edit->Machine Data and Edit->Base Length), the **Measurement** button should be pressed. Than a measured axis should be chosen (fig. 7.3) and than the optical path should be adjusted (see below). After the straightness of a chosen axis is measured a next axis should be chosen – Measurement->New Axis (fig. 7.4) When all the axes are measured, Flatness Plot button should be
pressed. The received flatness plot (fig. 7.1) may be saved, printed or exported to a text file (File->Save, File->Print or File->Export).

![Flatness Measurement Graph](image)

**FIG.7.4. CHANGING AXIS IN FLATNESS MEASUREMENT.**

**Optical path adjustment in the axis “1”.

The straightness measurement in the axis “1” is done with the optical components and in the way described in Chapter 6, *Straightness measurements.*

**Optical path adjustment in the axes: “3”, “6”, “8”.

During flatness measurements in the axes “3”, “6” and “8” an additional beam directing mirror **ZK1** is used. The way of using it is shown on Figure 7.5.
1. The diaphragm on the laser head set to the *Adjustment* position,
2. The beam directing mirror *ZK1* set 45° to the laser beam coming out from the head,
3. Place the angle interferometer *IK1* in the measured axis,
4. Set the diaphragm on the angle interferometer to the *Adjustment* position,
5. Change the position of the head so that the beam falls in the middle of upper interferometer’s diaphragm,
6. Set the diaphragm on the angle retro-reflector to the *Adjustment* position.
7. Moving the retro-reflector along the axis, change the position of the head so that the beam passing through the interferometer falls also in the middle of the retro-reflector’s diaphragm,

8. After changing the positions of the diaphragms on the interferometer and on the retro-reflector to Working positions, check if the return beam falls in the middle if measuring opening in the head. Do the check moving the retro-reflector along the axis. Corrections, if needed, can be made both changing the head or the interferometer position,

9. Set the diaphragm on the laser head to Working position and check if the level indicator on the display shows around 100%,

10. Now the straightness measurements, as described in Chapter 6, can be made.

Optical path adjustment in the axes: “5” and “7”

During flatness measurements in the axes “5” and “7” two beam directing mirrors ZK1 are used. The way of using them is shown on Figure 7.6.
FIG. 7.6. THE SET OF THE OPTICAL COMPONENTS USED IN STRAIGHTNESS MEASUREMENTS IN THE AXES: “5” AND “7”

1. The diaphragm on the laser head set to the *Adjustment* position,
2. The first beam-directing mirror ZK1 set 45° to the laser beam coming out from the head. The position of the laser head should be regulated in a way that the beam reflected from the first mirror runs parallel to the axis “3” and falls on the second beam-directing mirror. The second mirror is set 45° to the first one,
3. Changing the position and the angle of the second mirror direct the reflected beam along the axes “5” or “7” in a way the beam is parallel to the axis,
4. Place the angle interferometer in magnetic holder of the second mirror and set it in the optical path,
FLATNESS MEASUREMENTS

5. Set the diaphragm on the angle interferometer to the Adjustment position,
6. Change the position of the head so that the beam falls in the middle of upper interferometer’s diaphragm,
7. Set the diaphragm on the angle retro-reflector to the Adjustment position,
8. Moving the retro-reflector along the axis, change the position of the head so that the beam passing through the interferometer falls also in the middle of the retro-reflector’s diaphragm,
9. After changing the positions of the diaphragms on the interferometer and on the retro-reflector to Working positions, check if the return beam falls in the middle if measuring opening in the head. Do the check moving the retro-reflector along the axis. Corrections, if needed, can be made both changing the head or the interferometer position,
10. Set the diaphragm on the laser head to Working position and check if the level indicator on the display shows around 100%,
11. Now the straightness measurements, as described in Chapter 6, can be made.

Optical path adjustment in the axes: “2” and “4”

Similar to previously described, during flatness measurements in the axes “2” and “4” two beam directing mirrors ZK1 are used. The difference is that the angle of the second mirror usually differs from 45°. The way of using them is shown on Figure 7.7.
1. The diaphragm on the laser head set to the *Adjustment* position,
2. The first beam-directing mirror *ZK1* set 45° to the laser beam coming out from the head. The position of the laser head should be regulated in a way that the beam reflected from the first mirror runs parallel to the axis “3” and falls on the second beam-directing mirror. The second mirror is set 45° to the first one,
3. Changing the position and the angle of the second mirror direct the reflected beam along the axis “4” in a way the beam is parallel to the axis,
4. Place the angle interferometer in magnetic holder of the second mirror and set it in the optical path,
5. Set the diaphragm on the angle interferometer to the *Adjustment* position,

6. Change the position of the head so that the beam falls in the middle of upper interferometer’s diaphragm,

7. Set the diaphragm on the angle retro-reflector to the *Adjustment* position,

8. Moving the retro-reflector along the axis, change the position of the head so that the beam passing through the interferometer falls also in the middle of the retro-reflector’s diaphragm,

9. After changing the positions of the diaphragms on the interferometer and on the retro-reflector to *Working* positions, check if the return beam falls in the middle if measuring opening in the head. Do the check moving the retro-reflector along the axis. Corrections, if needed, can be made both changing the head or the interferometer position,

10. Set the diaphragm on the laser head to *Working* position and check if the level indicator on the display shows around 100%,

11. Now the straightness measurements, as described in Chapter 6, can be made.

In the case of the measurements in the axis “2”, the path adjustment procedure is the same as described above. The only difference is that the first mirror, as not needed, is not used.
Straightness/squareness measurement highlight any bending component or overall misalignment in the guideways of a machine. This could be a result of a wear in guideways, an accident or poor machine foundations. The straightness/squareness errors will have a direct effect on a machine geometry and as the result on machining accuracy. The quick assessment of the machine geometry is one of the most important action required when the machine is mounted on the foundation.

The geometry measurements are one of the most time consuming measurements, the commonly used Wollastone prism optics is expensive and very difficult to adjust. Operation of the system with the Wollastone prism optics require high skilled personnel. There are three methods of straightness measurement: with angular optics, with Wollastone prism and with 3D method. The method with the angular optics was presented in section ANGULAR MEASUREMENT. The optics with the Wollastone prism is supplied optionally. The method 3D of straightness measurement don’t require any additional optics.

For squareness measurement one additional optical element is necessary – the optical square etalon. The straightness of the movement is measured by measuring of the position of the reference and position of the measuring beams returning to the laser head. 3D measurements offer unique possibility of measurements of straightness in two dimension in one measurement. This significantly shortens the measurement time. Besides the 3D straightness measurement are done at the same time when the positioning measurements.
After finishing the positioning cycle one can view the results of the straightness just by pressing “Straightness” on positioning screen. One could also measure the straightness in **Straightness** option chosen from the main menu. For 3D measurements one have to choose the 3D method of measurement from the “Measurement” menu or from the **Config** menu (on the main screen). The straightness measurement software procedure are the same like for straightness measurements described in “ANGULAR MEASUREMENT” section. In Fig. 8.1 the print screen made during the measuring process is presented. The automatic option of the measurement was chosen. In the left black rectangle one can see the position of the retro-reflector in mm, while in the upper and lower black rectangle the horizontal and vertical shift in micrometers.

**FIG. 8.1 THE PRINT SCREEN OF STRAIGHTNESS MEASUREMENT**
The result of the measurements are presented in Fig.8.2. The upper trace shows the straightness for the horizontal axis and the lower one the straightness of the vertical axis. The parameter $D_s$ represent the straightness error. And point fit method was chosen for plotting the result and for calculating of the straightness error.

![Graphs showing straightness measurements](image)

**FIG. 8.2 THE RESULTS OF STRAIGHTNESS MEASUREMENTS.**

The accuracy of the straightness measurements depends on the precision of the adjustment of the measured axis. It is recommended that the position of the crosses during adjustment (as seen on the Display screen) procedure to be set to the center of the screen (zero position). Vibrations of the base where the tripod is placed and air density fluctuations are the source of noise that lower accuracy of the measurement. When required accuracy of straightness measurement for
tested machine is not satisfactory one have to proceed to measurements with the use of angular optics or with the Wollastone prism.
The laser measurement system LP30-3D is capable of detecting machine vibrations in the frequency range from 0 to 500 Hz. For these measurements an element set for linear measurements is used i.e.: a PC computer, a laser head with a power supply, a stand Tripod, magnetic holders (one UM1 and one UM2), a linear interferometer IL1, and a linear retro-reflector RL1. The Environmental Compensation Unit - (ECU) and the temperature sensors do not have to be used. The optical path should be adjusted as shown in Chapter 4.

To obtain correct results, a point of attaching the retro-reflector to the corpse of a measured machine must be carefully chosen. If the point is chosen improperly than, instead of a sought frequency $f$, a multiple frequencies $n*f$ appear (where $n=1,2,...$) on the FFT chart. For that reason the retro-reflector must not be in theses measurements used with the magnetic holder UM1. It must be also remembered that the system measures the vibration only in the axis of the optical path. Any vibrations in perpendicular axes do not influence the measurement (see fig8.1). An example of a properly attached retro-reflector is shown on fig. 8.2.
FIG. 8.1. VIBRATION MEASUREMENT IN DIFFERENT AXES.

FIG. 8.2. EXAMPLE OF PROPERLY ATTACHED RETRO-REFLECTOR.
Measurements

After adjusting the optical path and choosing FFT option from Main Menu a window, as shown on fig.8.3 appears. The most important parts of this window are: time diagram, frequency diagram and radio buttons (on the right side). Before measurements a machine data may be set (Edit->Machine Data). The measurement starts after pressing the Measurement button. Then appears the Measurement Window (see fig.8.3) that shows two progress bars – the upper (blue) one shows the progress in measurement; the lower (green) one shows progress in sending data to the computer. The measurement is in progress when the upper bar is in the range of 0-100% (it lasts approx. 12s)!

![FIG.8.3. VIBRATION MEASUREMENT WINDOW.](image)

When both the measurement and the transmission are done, the measurement results are presented on the time diagram and its FFT analysis on the frequency diagram (fig.8.4). The results can be saved, printed or exported (menu File). With the use of radio buttons the type of input data may be chosen,
i.e. whether amplitude of Distance, Velocity or Acceleration is important. In the frequency diagram not only the amplitude of vibration frequencies may be displayed, but also their phase, and real and imaginary part of the vibration. The check buttons in the bottom right of the window allow to change the vertical scale of the frequency diagram to logarithmic and to eliminate a DC offset.

![Frequency Diagram](image)

**FIG.8.4. EXAMPLARY VIBRATION MEASUREMENT RESULTS.**

What may be confusing in obtained results are different amplitudes of frequencies on the frequency diagram after changing from Distance to Velocity and to Acceleration, fig. 8.5. It happens so, accordingly to the theory, from which results:

\[ E_{An} \approx f_n \cdot E_{Vn} \]
\[ E_{Dn} \approx f_n \cdot E_{An} \]

Where:

- \( E_{Dn} \) – amplitude of n-th frequency when Distance is chosen;
- \( E_{Vn} \) – amplitude of n-th frequency when Velocity is chosen;
- \( E_{An} \) – amplitude of n-th frequency when Acceleration is chosen;
- \( f_n \) – n-th frequency.
**FIG.8.5.** DIFFERENT FREQUENCIES’ AMPLITUDES IN DEPENDANCE ON .
System specifications

<table>
<thead>
<tr>
<th>Measurement</th>
<th>Range</th>
<th>Resolution</th>
<th>Accuracy</th>
</tr>
</thead>
<tbody>
<tr>
<td>Distance</td>
<td>0 – 30 m</td>
<td>0,01 µm (0,001 µm)</td>
<td>0,41 µm/m</td>
</tr>
<tr>
<td>Velocity</td>
<td>0 – 0,3 m/s (0,1 m/s)</td>
<td>0.25 µm/s</td>
<td>0,1 %</td>
</tr>
<tr>
<td>Angular</td>
<td>0 – 3600 arcsec</td>
<td>0,04 arcsec</td>
<td>± 0,2 %</td>
</tr>
<tr>
<td>Straightness measurement (with angular optics)</td>
<td>0 – 12 m</td>
<td>0,02 µm (for 100 mm base)</td>
<td>± 1 %</td>
</tr>
<tr>
<td>Flatness</td>
<td>0 – 12 m</td>
<td>0,02 µm (for 100 mm base)</td>
<td>± 0,5 %</td>
</tr>
<tr>
<td></td>
<td>Vertical range ±2 mm</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Straightness measurement (with wollastone prism)</td>
<td>0 – 3 m</td>
<td>0,5 µm</td>
<td>± 1 %±(0,5±0,15L²) µm</td>
</tr>
<tr>
<td>Straightness measurement 3D</td>
<td>0-10 m</td>
<td>0,1 µm</td>
<td>(3± 2 x L) µm</td>
</tr>
<tr>
<td>Squareness</td>
<td>± 1000 arcsec</td>
<td>0,4arcsec</td>
<td>± 1 % ± (1,5 arcsec)</td>
</tr>
<tr>
<td>Rotary measurements</td>
<td>± 5 °</td>
<td>0,04 arcsec</td>
<td>± 0,2 %</td>
</tr>
</tbody>
</table>

L = axis length in meters
* - for resolution 1 nm.
Laser head

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Specification</th>
</tr>
</thead>
<tbody>
<tr>
<td>Laser type</td>
<td>Zeeman HeNe laser with frequency stabilization</td>
</tr>
<tr>
<td>Heating time</td>
<td>Approx. 20 min</td>
</tr>
<tr>
<td>Wavelength (vacuum)</td>
<td>632,991354 nm</td>
</tr>
<tr>
<td>Wavelength accuracy</td>
<td>± 0,02 ppm</td>
</tr>
<tr>
<td>Short time stability</td>
<td>± 0,002 ppm (1 hour)</td>
</tr>
<tr>
<td>Output power</td>
<td>400 µW</td>
</tr>
<tr>
<td>Beam diameter</td>
<td>8 mm</td>
</tr>
<tr>
<td>Distance between out- and ingoing beam</td>
<td>12,7 mm</td>
</tr>
<tr>
<td>Laser head dimensions</td>
<td>60x60x245 mm</td>
</tr>
<tr>
<td>Net weight</td>
<td>1500 g</td>
</tr>
<tr>
<td>Safety class</td>
<td>Class 2 Laser product according to PN-91/T-06700</td>
</tr>
</tbody>
</table>

System work conditions

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Specification</th>
</tr>
</thead>
<tbody>
<tr>
<td>Temperature range</td>
<td>10 – 35 °C</td>
</tr>
<tr>
<td>Humidity range</td>
<td>10 – 90 %</td>
</tr>
</tbody>
</table>

Power supply

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Specification</th>
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</thead>
<tbody>
<tr>
<td>Voltage</td>
<td>90-230 VAC, 50-60 Hz</td>
</tr>
<tr>
<td>Power</td>
<td>35 W (during heating) 10 W (work)</td>
</tr>
</tbody>
</table>

PC interface

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Specification</th>
</tr>
</thead>
<tbody>
<tr>
<td>Type</td>
<td>RS 232C, USB</td>
</tr>
<tr>
<td>Data rate</td>
<td>57 600 bps (RS 232)</td>
</tr>
</tbody>
</table>
Environment compensation

Wavelength compensation

<table>
<thead>
<tr>
<th>Manual</th>
<th>Environments parameters entered from keyboard</th>
</tr>
</thead>
<tbody>
<tr>
<td>Automatic</td>
<td>With the use of the Environmental Compensation Unit - (ECU) .</td>
</tr>
</tbody>
</table>

Parameters of the Environmental Compensation Unit - (ECU) compensation

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Specification</th>
</tr>
</thead>
<tbody>
<tr>
<td>Air temperature</td>
<td>Range 0 – 40 °C, accuracy 0,1 °C</td>
</tr>
<tr>
<td>Pressure</td>
<td>Range 940 – 1060 hPa, accuracy 1 hPa</td>
</tr>
<tr>
<td>Humidity</td>
<td>Range 10 – 90 %, accuracy 10 %</td>
</tr>
<tr>
<td>Time constants</td>
<td>Temperature 3 s, pressure 2s, humidity 30 s</td>
</tr>
<tr>
<td>Dimension</td>
<td>Ø50x55 mm</td>
</tr>
<tr>
<td>Net weight</td>
<td>100 g</td>
</tr>
</tbody>
</table>

Material temperature compensation

<table>
<thead>
<tr>
<th>Manual</th>
<th>Temperature of material entered from keyboard</th>
</tr>
</thead>
<tbody>
<tr>
<td>Automatic</td>
<td>With the use of 1 to 3 temperature sensors .</td>
</tr>
<tr>
<td>Temperature sensor</td>
<td>Pt-1000 in oil resistant casing</td>
</tr>
<tr>
<td>Time constant</td>
<td>5 s</td>
</tr>
<tr>
<td>Net weight</td>
<td>50 g</td>
</tr>
</tbody>
</table>

Our products are subject to continuous further development and improvement. Subject to technical changes without prior notice.